

ENERGY PRINCIPLE

Steady Flow Energy Equation

For steady flow, the flow accumulation equal zero and if the velocity distribution is constant, then

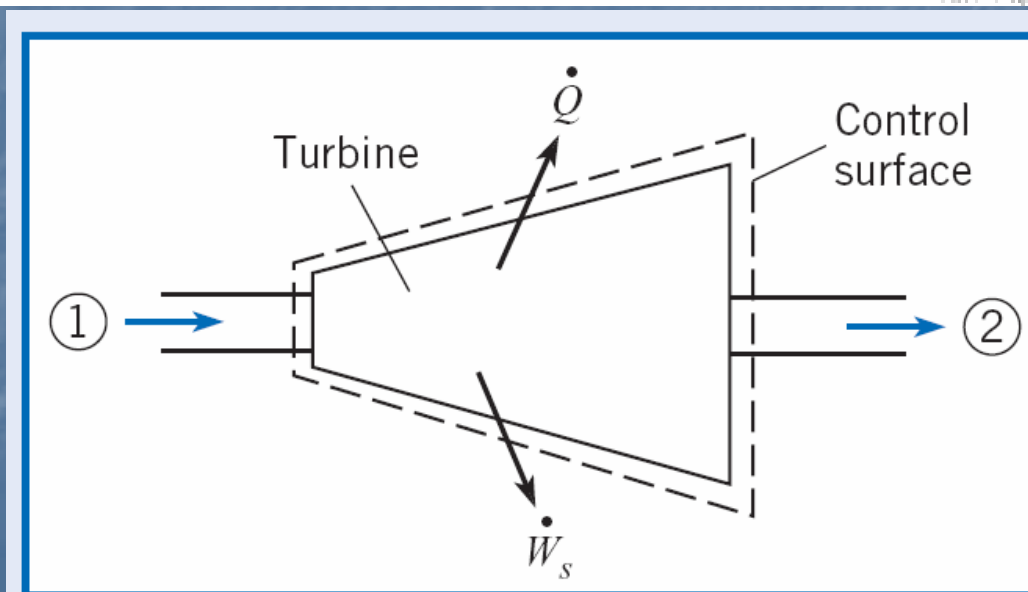
the Eqn. $\dot{Q} - \dot{W}_s = \frac{d}{dt} \int_{CV} (u + \frac{v^2}{2} + gz) \rho dQ + \int_{CS} (h + \frac{v^2}{2} + gz) \rho \mathbf{V} \cdot d\mathbf{A}$ becomes

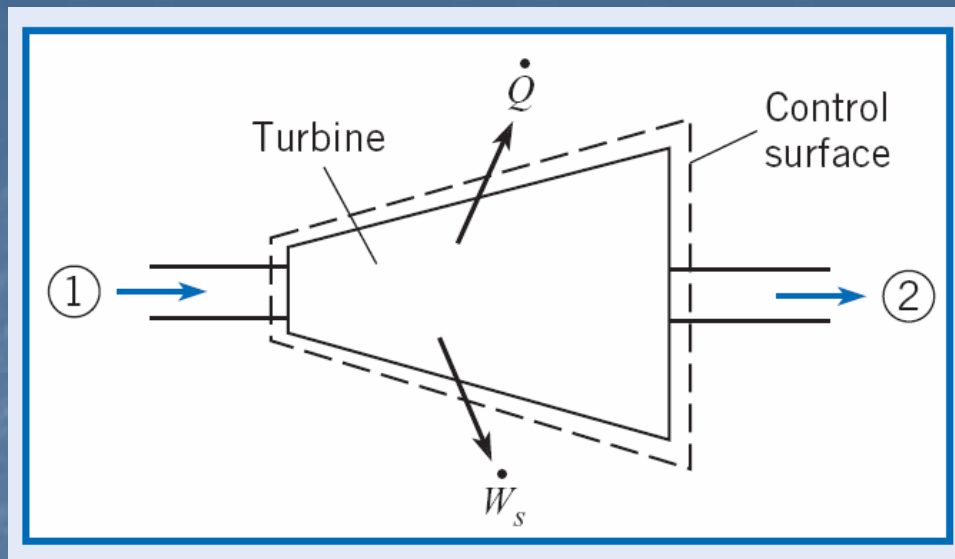
$$\dot{Q} - \dot{W}_s = \sum_{CS} \dot{m}_{out} \left(\frac{V^2}{2} + gz + h \right)_{out} - \sum_{CS} \dot{m}_{in} \left(\frac{V^2}{2} + gz + h \right)_{in}$$

Example (7.1)

A steam turbine receives superheated steam at 1.4 MPa absolute and 400°C, which corresponds to a specific enthalpy of 3121 kJ/kg. The steam leaves the turbine at 101 kPa absolute and 100°C, for which the specific enthalpy is 2676 kJ/kg. The steam enters the turbine at 15 m/s and exits at 60 m/s. The elevation difference between entry and exit ports is negligible. The heat lost through the turbine wall is 7600 kJ/h. Calculate the power output if the mass flow through the turbine is 0.5 kg/s.

Solution First sketch the general layout of the turbine, indicating the inlet and outlet velocities, shaft work, and heat transfer, as shown.





Given: $h_1 = 3121 \frac{\text{kJ}}{\text{kg}}$, $h_2 = 2676 \frac{\text{kJ}}{\text{kg}}$, $V_{in} = 15 \frac{\text{m}}{\text{s}}$, $V_{out} = \frac{\text{m}}{\text{s}}$, $\dot{Q} = 7600 \frac{\text{kJ}}{\text{kg}}$, $z_1 = z_2$,

$$\dot{m} = 0.5 \frac{\text{kg}}{\text{sec}}$$

Find: \dot{W}_{Shaft} ?

Applying the steady flow energy equation

$$\dot{Q} - \dot{W}_S = \sum_{CS} \dot{m}_{out} \left(\frac{V^2}{2} + gz + h \right)_{out} - \sum_{CS} \dot{m}_{in} \left(\frac{V^2}{2} + gz + h \right)_{in}$$

$$(gz)_{out} = (gz)_{in} = 0, \quad \dot{m}_{in} = \dot{m}_{out} = \dot{m},$$

$$\dot{W}_S = \dot{Q} + \dot{m} \left(h_1 - h_2 + \frac{V_1^2}{2} - \frac{V_2^2}{2} \right)$$

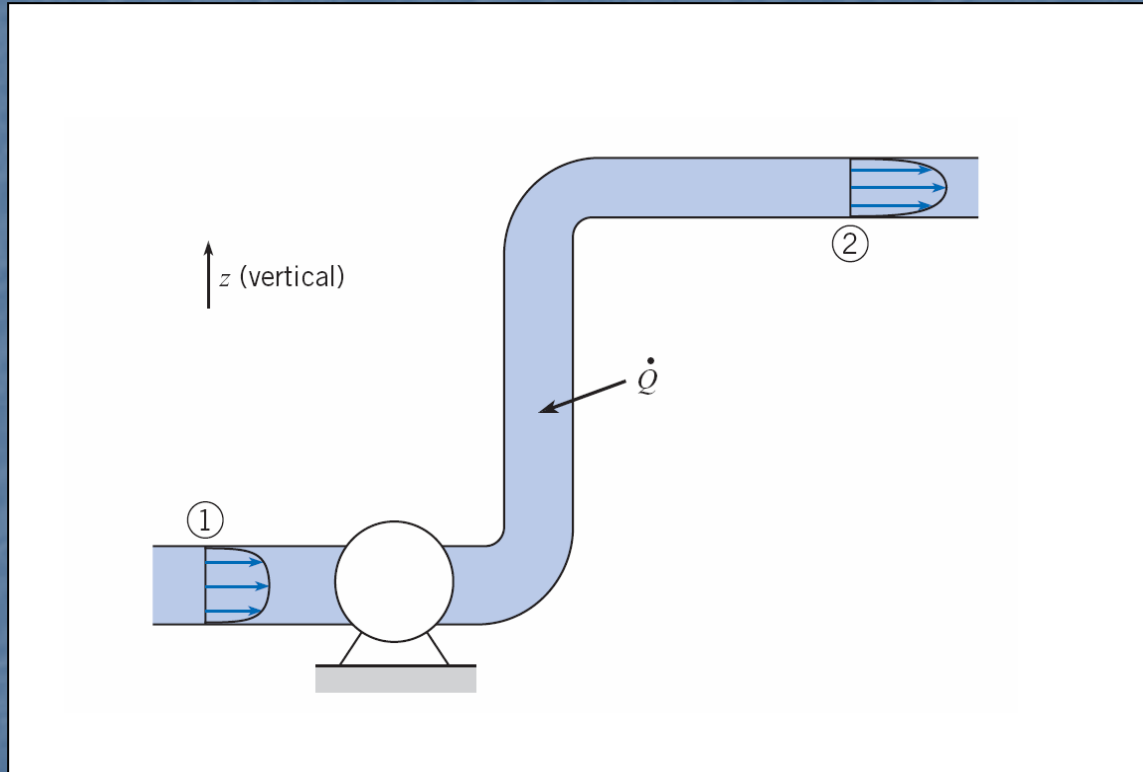
$$\begin{aligned} \dot{W}_S &= \frac{-7600}{3600} \frac{\text{kJ}}{\text{h}} \frac{\text{h}}{\text{s}} + 0.5 \frac{\text{kg}}{\text{s}} \left[\frac{15^2 - 60^2}{2 \times 10^3} \frac{\text{kJ}}{\text{kg}} + (3121 - 2676) \frac{\text{kJ}}{\text{kg}} \right] \\ &= -2.11 + 0.5(-1.69 + 445) = 220 \frac{\text{kJ}}{\text{s}} = 220 \text{ kW} \end{aligned}$$

$$\dot{W}_S = 220 \text{ kW}$$

Note : (\dot{Q}) is negative as heat flow out of the system

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Energy Equation for Steady Flow of an Incompressible Fluid in a pipe



Consider the flow as shown above

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The general Energy Eqn. is written as

$$\dot{Q} - \dot{W}_s = \frac{d}{dt} \int_{CV} \left(u + \frac{v^2}{2} + gz \right) \rho dQ + \int_{CS} \left(h + \frac{v^2}{2} + gz \right) \rho \mathbf{V} \cdot d\mathbf{A}$$

The energy accumulation term $\frac{d}{dt} \int_{CV} \left(u + \frac{v^2}{2} + gz \right) \rho dQ = 0$ (Steady Flow)

$$\dot{Q} - \dot{W}_s = \int_{CS} \left(h + \frac{v^2}{2} + gz \right) \rho \mathbf{V} \cdot d\mathbf{A} \quad \text{where } \left(h = \frac{p}{\rho} + u \right)$$

Applying the above equation between section 1 & 2, we have,

$$\dot{Q} - \dot{W}_s = \int_{A2} \left(h_2 + \frac{V_2^2}{2} + gz_2 \right) \rho V_2 dA_1 - \int_{A1} \left(h_1 + \frac{V_1^2}{2} + gz_1 \right) \rho V_1 dA_1$$

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The term enthalpy = $h = \left(u + \frac{p}{\rho} \right)$

$$\dot{Q} - \dot{W}_s = \int_{A_2} \left(\frac{p_2}{\rho} + u_2 + \frac{V_2^2}{2} + gz_2 \right) \rho V_2 dA_1 - \int_{A_1} \left(\frac{p_1}{\rho} + u_1 + \frac{V_1^2}{2} + gz_1 \right) \rho V_1 dA_1$$

$$\dot{Q} - \dot{W}_s + \int_{A_1} \left(\frac{p_1}{\rho} + gz_1 + u \right) \rho V_1 dA_1 + \int_{A_1} \frac{\rho V_1^3}{2} dA_1 = \int_{A_2} \left(\frac{p_2}{\rho} + gz_2 + u_2 \right) \rho V_2 dA_1 + \int_{A_2} \frac{\rho V_2^3}{2} dA_2$$

It is common to express the term $\int \frac{\rho V^3}{2} dA = \alpha \left(\frac{\bar{V}^3}{2} \right) A$

Substituting for $\int \frac{\rho V^3}{2} dA = \alpha \left(\frac{\bar{V}^3}{2} \right) A$ in Eqn. above and dividing through by \dot{m}

$$\frac{1}{\dot{m}} (\dot{Q} - \dot{W}_s) + \left(\frac{p_1}{\rho} + gz_1 + u_1 + \alpha_1 \frac{\bar{V}_1^2}{2} \right) = \left(\frac{p_2}{\rho} + gz_2 + u_2 + \alpha_2 \frac{\bar{V}_2^2}{2} \right)$$

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The coefficients (α_1, α_2) are called kinetic energy correction factor and can be evaluated as follows :

$$\alpha \frac{\rho \bar{V}^3 A}{2} = \int_A \frac{\rho V^3 dA}{2}$$

$$\alpha = \frac{1}{A} \int_A \left(\frac{V}{\bar{V}} \right)^3 dA$$

$\alpha = 1$ *Velocity is uniform*

$\alpha > 1$ *Velocity is non – uniform*

$\alpha = 2$ *Laminar Flow*

$\alpha = 1.05$ *Turbulent Flow*

**END OF LECTURE
(2)**